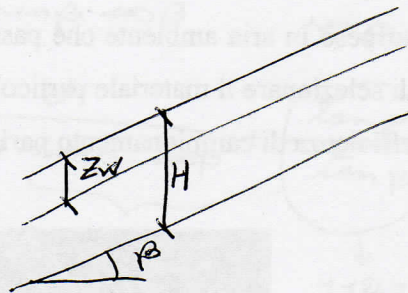


Un pendio indefinito è costituito da uno strato di terreno ( $\gamma = 19 \text{ kN/m}^3$ ;  $\gamma_{\text{sat}} = 19,5 \text{ kN/m}^3$ ) di spessore  $h = 4 \text{ m}$  e  $\beta = 30^\circ$ . Determinare il FS del pendio nelle seguenti condizioni:

- terreno asciutto;
- livello di falda coincidente con il piano campagna e moto di filtrazione parallelo al pendio;
- livello di falda ad  $1 \text{ m}$  ( $z_w = 1 \text{ m}$ ) dal piano campagna e moto di filtrazione parallelo al pendio;
- pendio sommerso.

Per la caratterizzazione geotecnica del terreno si può fare riferimento ai risultati di prove di taglio riportati in tabella.

	$\sigma'_i \text{ (kPa)}$	$\tau_i \text{ (kPa)}$	$\sigma_i'^2$	$\tau_i \cdot \sigma'_i$
1° prov.	50	50	2500	2500
2° prov.	100	78	10000	7800
3° prov.	150	115	22500	17250
$\Sigma$	300	243	35000	27550



Applico il metodo dei minimi quadrati:

$$c' = \frac{\Sigma \tau_i \cdot \Sigma (\sigma'_i)^2 - \Sigma \sigma'_i \cdot \Sigma (\sigma'_i \cdot \tau_i)}{n \Sigma (\sigma'_i)^2 - (\Sigma \sigma'_i)^2}$$

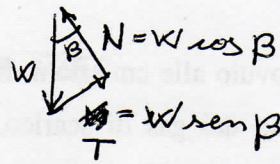
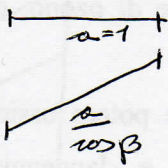
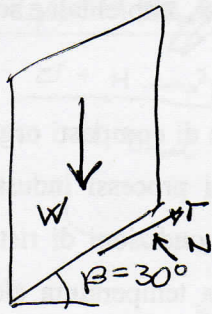
$n = n^\circ \text{ prove}$

$$\tan \phi' = \frac{n \Sigma (\sigma'_i \cdot \tau_i) - \Sigma \sigma'_i \cdot \Sigma \tau_i}{n \Sigma (\sigma'_i)^2 - (\Sigma \sigma'_i)^2}$$

$$c' = \frac{243 \cdot 35000 - 300 \cdot 27550}{3 \cdot 35000 - 300^2} = 16 \text{ kPa}$$

$$\tan \phi' = \frac{3 \cdot 27550 - 300 \cdot 243}{3 \cdot 35000 - 300^2} = 0,65 \Rightarrow \phi' = 33^\circ$$

a) terreno scivolato



$$\sigma = \frac{N}{A} = \frac{W \cos \beta}{\frac{a}{\cos \beta}} = W \cos^2 \beta$$

$$\tau = \frac{T}{A} = \frac{W \sin \beta}{\frac{a}{\cos \beta}} = W \sin \beta \cdot \cos \beta$$

$$W = \gamma \cdot H$$

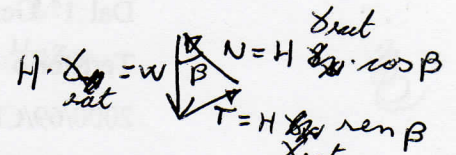
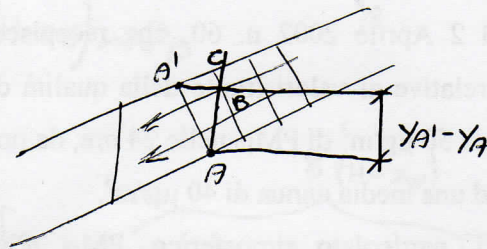
$$F_s = \frac{c' + \sigma' \tan \phi'}{\tau} = \frac{c' + (\sigma - \mu) \tan \phi'}{\tau}$$

$$F_s = \frac{c' + [\gamma \cdot H \cos^2 \beta] \tan \phi'}{\gamma \cdot H \sin \beta \cos \beta} = \frac{c'}{\gamma \cdot H \sin \beta \cdot \cos \beta} + \frac{\tan \phi' \cos \beta}{\sin \beta}$$

$$= \frac{c'}{\gamma \cdot H \cdot \sin \beta \cdot \cos \beta} + \frac{\tan \phi'}{\tan \beta}$$

1,1248  
1,0789

b) PF = PC



$$\sigma = \frac{N}{A} = \frac{H \gamma \cos \beta}{\frac{z}{\cos \beta}} = H \gamma$$

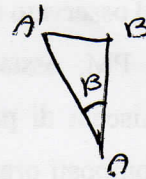
$$\tau = \frac{T}{A} = \frac{H \gamma \sin \beta}{\frac{z}{\cos \beta}}$$

$$H_A = H_{A'}$$

$$z_A + \frac{\mu_A}{\gamma_w} = z_{A'} + \frac{\mu_{A'}}{\gamma_w} = 0$$

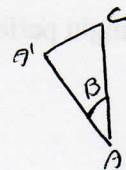
$$\Rightarrow \mu_A = \gamma_w (z_{A'} - z_A) = \underbrace{AB}_{H \cos^2 \beta}$$

$$\mu_A = \gamma_w \cdot H \cdot \cos^2 \beta$$



$$AB = AA' \cos \beta$$

$$AA' = \frac{AB}{\cos \beta}$$



$$AA' = AC \cos \beta$$

$$H$$

$$F_s = \frac{c' + (H \gamma \cos^2 \beta - \gamma_w H \cos^2 \beta) \tan \phi'}{H \gamma \sin \beta \cos \beta} = 1,58$$

1,1248

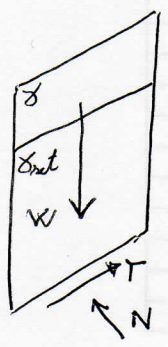
~~$F_s = \frac{c' + H \cos^2 \beta \delta' \tan \phi}{H \delta_{nat} \sin \beta \cos \beta}$~~

$$F_s = \frac{c' + H \cos^2 \beta \delta' \tan \phi}{H \delta_{nat} \sin \beta \cos \beta} = 0,956$$

0,1045

37,557

c)



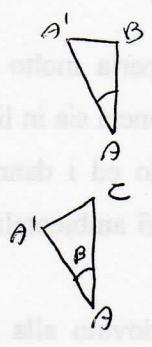
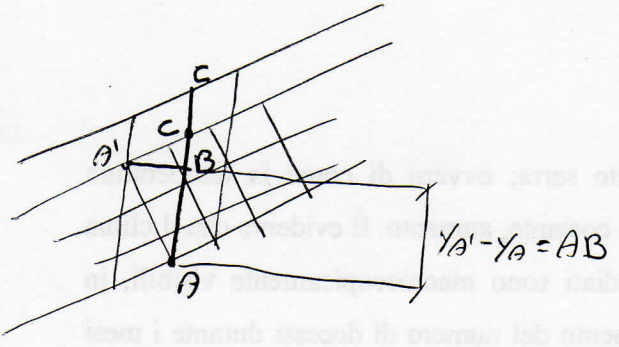
$$W = \delta \cdot z_w + \delta_{nat}(H - z_w)$$

$$N = W \cos \beta = [\delta \cdot z_w + \delta_{nat}(H - z_w)] \cos \beta$$

$$T = W \sin \beta = [\delta \cdot z_w + \delta_{nat}(H - z_w)] \sin \beta$$

$$\sigma = \frac{N}{A} = \frac{z_w}{\cos \beta} = [\delta \cdot z_w + \delta_{nat}(H - z_w)] \cos^2 \beta$$

$$\tau = \frac{T}{A} = [\delta \cdot z_w + \delta_{nat}(H - z_w)] \sin \beta \cdot \cos \beta$$



$$AB = AA' \cos \beta$$

$$AA' = AC \cos \beta$$

↓

$$H - z_w$$

$$AB = (H - z_w) \cos^2 \beta$$

$$u_A = \delta_w \cdot (H - z_w) \cos^2 \beta$$

$$F_s = \frac{c' + \cos^2 \beta [\delta \cdot z_w + \delta_{nat}(H - z_w) - \delta_w(H - z_w)] \tan \phi}{\delta z_w + \delta_{nat}(H - z_w) \sin \beta \cos \beta} = 0,958$$

42,663